

Specification Guide

Notices

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Documentation is updated periodically. For the latest information about this analyzer, including firmware upgrades, application information, and product information, see the following URL:

http://www.keysight.com/find/cxa

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Information on preventing analyzer damage can be found at:

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Specification Guide

1 Keysight CXA Signal Analyzer

This chapter contains the specifications for the core signal analyzer. The specifications and characteristics for the measurement applications and options are covered in the chapters that follow.

Definitions and Requirements

This book contains signal analyzer specifications and supplemental information. The distinction among specifications, typical performance, and nominal values are described as follows.

Definitions

- Specifications describe the performance of parameters covered by the product warranty (temperature = 0 to 55°C, also referred to as "Full temperature range" or "Full range", unless otherwise noted.
- 95th percentile values indicate the breadth of the population (»2s) of performance tolerances expected to be met in 95% of the cases with a 95% confidence, for any ambient temperature in the range of 20 to 30°C. In addition to the statistical observations of a sample of instruments, these values include the effects of the uncertainties of external calibration references. These values are not warranted. These values are updated occasionally if a significant change in the statistically observed behavior of production instruments is observed.
- Typical describes additional product performance information that is not covered by the product warranty. It is performance beyond specification that 80% of the units exhibit with a 95% confidence level over the temperature range 20 to 30°C. Typical performance does not include measurement uncertainty.
- Nominal values indicate expected performance, or describe product performance that is useful in the application of the product, but is not covered by the product warranty.

Conditions Required to Meet Specifications

The following conditions must be met for the analyzer to meet its specifications.

- The analyzer is within its calibration cycle. See the General section of this chapter.
- Under auto couple control, except that Auto Sweep Time Rules = Accy.
- For signal frequencies < 10 MHz, DC coupling applied (*Option 513/526* only).
- Any analyzer that has been stored at a temperature range inside the allowed storage range but outside the allowed operating range must be stored at an ambient temperature within the allowed operating range for at least two hours before being turned on.
- The analyzer has been turned on at least 30 minutes with Auto Align set to Normal, or, if Auto Align is set to Off or Partial, alignments must have been run recently enough to prevent an Alert message. If the Alert condition is changed from "Time and Temperature" to one of the disabled duration choices, the analyzer may fail to meet specifications without informing the user. If Auto Align is set to Light, performance is not warranted, and nominal performance will degrade to become a factor of 1.4 wider for any specification subject to alignment, such as amplitude tolerances.

Certification

Keysight Technologies certifies that this product met its published specifications at the time of shipment from the factory. Keysight Technologies further certifies that its calibration measurements are traceable to the United States National Institute of Standards and Technology, to the extent allowed by the Institute's calibration facility, and to the calibration facilities of other International Standards Organization members.

Keysight CXA Signal Analyzer Frequency and Time

a. N is the LO multiplication factor.

b. In the band overlap regions, take option 513/526 for example, 2.95 to 7.5 GHz, the analyzer may use either band for measurements, in this example Band 0 or Band 1. The analyzer gives preference to the band with the better overall specifications, but will choose the other band if doing so is necessary to achieve a sweep having minimum band crossings. For example, with CF = 2.98 GHz, with a span of 40 MHz or less, the analyzer uses Band 0, because the stop frequency is 3.0 GHz or less, allowing a span without band crossings in the preferred band. If the span is between 40 and 60 MHz, the analyzer uses Band 1, because the start frequency is above 2.95 GHz, allowing the sweep to be done without a band crossing in Band 1, though the stop frequency is above 3.0 GHz, preventing a Band 0 sweep without band crossing. With a span greater than 60 MHz, a band crossing will be required: the analyzer sweeps up to 3.0 GHz in Band 0; then executes a band crossing and continues the sweep in Band 1.

Specifications are given separately for each band in the band overlap regions. One of these specifications is for the preferred band, and one for the alternate band. Continuing with the example from the previous paragraph (2.98 GHz), the preferred band is band 0 (indicated as frequencies under 3.0 GHz) and the alternate band is band 1 (2.95 to 7.5 GHz). The specifications for the preferred band are warranted. The specifications for the alternate band are not warranted in the band overlap region, but performance is nominally the same as those warranted specifications in the rest of the band. Again, in this example, consider a signal at 2.98 GHz. If the sweep has been configured so that the signal at 2.98 GHz is measured in Band 1, the analysis behavior is nominally as stated in the Band 1 specification line (2.95 to 7.5 GHz) but is not warranted. If warranted performance is necessary for this signal, the sweep should be reconfigured so that analysis occurs in Band 0. Another way to express this situation in this example Band0/Band 1 crossing is this: The specifications given in the "Specifications" column which are described as "2.95 to 7.5 GHz" represent nominal performance from 2.95 to 3.0 GHz, and warranted performance from 3.0 to 7.5 GHz.

a. Calibration accuracy depends on how accurately the frequency standard was adjusted to 10 MHz. If the adjustment procedure is followed, the calibration accuracy is given by the specification "Achievable Initial Calibration Accuracy".

b. For periods of one year or more.

a. Calibration accuracy depends on how accurately the frequency standard was adjusted to 10 MHz. If the adjustment procedure is followed, the calibration accuracy is given by the specification "Achievable Initial Calibration Accuracy."

b. The specification applies after the analyzer has been powered on for 15 minutes.

c. Standby mode does not apply power to the oscillator. Therefore warm-up applies every time the power is turned on. The warm-up reference is one hour after turning the power on. Retracing also occurs every time the power is applied. The effect of retracing is included within the "Achievable Initial Calibration Accuracy" term of the Accuracy equation.

d. The achievable calibration accuracy at the beginning of the calibration cycle includes these effects:

1) Temperature difference between the calibration environment and the use environment

2) Orientation relative to the gravitation field changing between the calibration environment and the use environment

3) Retrace effects in both the calibration environment and the use environment due to turning the instrument power off. 4) Settability

Keysight CXA Signal Analyzer Frequency and Time

a. The warranted performance is only the sum of all errors under autocoupled conditions. Under non-autocoupled conditions, the frequency readout accuracy will nominally meet the specification equation, except for conditions in which the RBW term dominates, as explained in examples below. The nominal RBW contribution to frequency readout accuracy is 4% of RBW for RBWs from 1 Hz to 3 MHz (the widest autocoupled RBW), and 30% of RBW for the (manually selected) 4, 5, 6 and 8 MHz RBWs. *Example*: a 20 MHz span, with a 4 MHz RBW. The specification equation does not apply because the Span: RBW ratio is not autocoupled. If the equation did apply, it would allow 50 kHz of error (0.25%) due to the span and 200 kHz error (5%) due to the RBW. For this non-autocoupled RBW, the RBW error is nominally 30%, or 1200 kHz.

- b. Horizontal resolution is due to the marker reading out one of the trace points. The points are spaced by span/(Npts 1), where Npts is the number of sweep points. For example, with the factory preset value of 1001 sweep points, the horizontal resolution is span/1000. However, there is an exception: When both the detector mode is "normal" and the span > $0.25 \times (Npts - 1) \times RBW$, peaks can occur only in even-numbered points, so the effective horizontal resolution becomes doubled, or span/500 for the factory preset case. When the RBW is autocoupled and there are 1001 sweep points, that exception occurs only for spans > 750 MHz.
- c. In most cases, the frequency readout accuracy of the analyzer can be exceptionally good. As an example, Keysight has characterized the accuracy of a span commonly used for Electro-Magnetic Compatibility (EMC) testing using a source frequency locked to the analyzer. Ideally, this sweep would include EMC bands C and D and thus sweep from 30 to 1000 MHz. Ideally, the analysis bandwidth would be 120 kHz at -6 dB, and the spacing of the points would be half of this (60 kHz). With a start frequency of 30 MHz and a stop frequency of 1000.2 MHz and a total of 16168 points, the spacing of points is ideal. The detector used was the Peak detector. The accuracy of frequency readout of all the points tested in this span was with ±0.0032% of the span. A perfect analyzer with this many points would have an accuracy of ±0.0031% of span. Thus, even with this large number of display points, the errors in excess of the bucket quantization limitation were negligible.

a. Instrument conditions: RBW = 1 kHz, gate time = auto (100 ms), $S/N \ge 50$ dB, frequency = 1 GHz.

b. If the signal being measured is locked to the same frequency reference as the analyzer, the specified count accuracy is ± 0.100 Hz under the test conditions of footnote [a.](#page-13-2) This error is a noisiness of the result. It will increase with noisy sources, wider RBWs, lower S/N ratios, and source frequencies > 1 GHz.

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a. Delayed trigger is available with line, video, RF burst and external triggers.

a. The highest allowed mixer level depends on the attenuation and IF Gain. It is nominally -10 dBm + input attenuation for Preamp Off and IF Gain = Low.

b. Noise will limit trigger level range at high frequencies, such as above 13 GHz.

- a. The noise marker, band power marker, channel power and ACP all compute their results using the power bandwidth of the RBW used for the measurement. Power bandwidth accuracy is the power uncertainty in the results of these measurements due only to bandwidth-related errors. (The analyzer knows this power bandwidth for each RBW with greater accuracy than the RBW width itself, and can therefore achieve lower errors.) The warranted specifications shown apply to the Gaussian RBW filters used in swept and zero span analysis. There are four different kinds of filters used in the spectrum analyzer: Swept Gaussian, Swept Flattop, FFT Gaussian and FFT Flattop. While the warranted performance only applies to the swept Gaussian filters, because only they are kept under statistical process control, the other filters nominally have the same performance.
- b. Resolution Bandwidth Accuracy can be observed at slower sweep times than auto-coupled conditions. Normal sweep rates cause the shape of the RBW filter displayed on the analyzer screen to widen by nominally 6%. This widening declines to 0.6% nominal when the Swp Time Rules key is set to Accuracy instead of Normal. The true bandwidth, which determines the response to impulsive signals and noise-like signals, is not affected by the sweep rate.
- c. The RBW filters are implemented digitally, and the selectivity is designed to be 4.1:1. Verifying the selectivity with RBWs above 100 kHz becomes increasing problematic due to SNR affecting the -60 dB measurement.

a. Analysis bandwidth is the instantaneous bandwidth available around a center frequency over which the input signal can be digitized for further analysis or processing in the time, frequency, or modulation domain.

a. For FFT processing, the selected VBW is used to determine a number of averages for FFT results. That number is chosen to give roughly equival lay smoothing to VBW filtering in a swept measurement. For example, if VBW=0.1 x RBW, four FFTs are averaged to generate one result.

Amplitude Accuracy and Range

a. Reference level and off-screen performance: The reference level (RL) behavior differs from previous analyzers (except PSA) in a way that makes the Keysight CXA Signal Analyzer more flexible. In previous analyzers, the RL controlled how the measurement was performed as well as how it was displayed. Because the logarithmic amplifier in previous analyzers had both range and resolution limitations, this behavior was necessary for optimum measurement accuracy. The logarithmic amplifier in the CXA signal analyzer, however, is implemented digitally such that the range and resolution greatly exceed other instrument limitations. Because of this, the CXA signal analyzer can make measurements largely independent of the setting of the RL without compromising accuracy. Because the RL becomes a display function, not a measurement function, a marker can read out results that are off-screen, either above or below, without any change in accuracy. The only exception to the independence of RL and the way in which the measurement is performed is in the input attenuation setting: When the input attenuation is set to auto, the rules for the determination of the input attenuation include dependence on the reference level. Because the input attenuation setting controls the tradeoff between large signal behaviors (third-order intermodulation and compression) and small signal effects (noise), the measurement results can change with RL changes when the input attenuation is set to auto.

Frequency Response

Keysight CXA Signal Analyzer Amplitude Accuracy and Range

a. Signal frequencies between 18 and 26.5 GHz are prone to additional response errors due to modes in the Type-N connector used with frequency Option 526. With the use of Type-N to APC 3.5 mm adapter part number 1250-1744, there are nominally six such modes. The effect of these modes with this connector are included within these specifications.

b. For Sweep Type = FFT, add the RF flatness errors of this table to the IF Frequency Response errors. An additional error source, the error in switching between swept and FFT sweep types, is nominally ±0.01 dB and is included within the "Absolute Amplitude Error" specifications.

a. The IF frequency response includes effects due to RF circuits such as input filters, that are a function of RF frequency, in addition to the IF pass-band effects.

b. Signal frequencies between 18 and 26.5 GHz are prone to additional response errors due to modes in the Type-N connector used with frequency Option 526. With the use of Type-N to APC 3.5 mm adapter part number 1250-1744, there are nominally six such modes. These modes cause nominally up to –0.35 dB amplitude change, with phase errors of nominally up to $\pm 1.2^\circ$.

c. The maximum error at an offset (f) from the center of the FFT width is given by the expression \pm [Midwidth Error + (f \times Slope)], but never exceeds ±Max Error. Usually, the span is no larger than the FFT width in which case the center of the FFT width is the center frequency of the analyzer. When the analyzer span is wider than the FFT width, the span is made up of multiple concatenated FFT results, and thus has multiple centers of FFT widths so the f in the equation is the offset from the nearest center. These specifications include the effect of RF frequency response as well as IF frequency response at the worst case center frequency. Performance is nominally three times better than the maximum error at most center frequencies.

d. The specification does not apply for frequencies greater than 3.0 MHz from the center in FFT Widths of 7.2 to 8 MHz.

e. The "RMS" nominal performance is the standard deviation of the response relative to the center frequency, integrated across a 10 MHz span. This performance measure was observed at a single center frequency in each harmonic mixing band, which is representative of all center frequencies; the observation center frequency is not the worst case center frequency.

a. Signal frequencies between 18 and 26.5 GHz are prone to additional response errors due to modes in the Type-N connector used with frequency Option 526. With the use of Type-N to APC 3.5 mm adapter part number 1250-1744, there are nominally six such modes. These modes cause nominally up to -0.35 dB amplitude change, with phase errors of nominally up to ±1.2°.

b. The listed performance is the r.m.s. of the phase deviation relative to the mean phase deviation from a linear phase condition, where the r.m.s. is computed over the range of offset frequencies and center frequencies shown.

Keysight CXA Signal Analyzer Amplitude Accuracy and Range

a. Absolute amplitude accuracy is the total of all amplitude measurement errors, and applies over the following subset of settings and conditions: $1 \text{ Hz} \leq \text{RBW} \leq 1 \text{ MHz}$; Input signal -10 to -50 dBm; Input attenuation 10 dB; span \lt 5 MHz (nominal additional error for span \geq 5 MHz is 0.02 dB); all settings auto-coupled except Swp Time Rules = Accuracy; combinations of low signal level and wide RBW use VBW \leq 30 kHz to reduce noise.

 This absolute amplitude accuracy specification includes the sum of the following individual specifications under the conditions listed above: Scale Fidelity, Reference Level Accuracy, Display Scale Switching Uncertainty, Resolution Bandwidth Switching Uncertainty, 50 MHz Amplitude Reference Accuracy, and the accuracy with which the instrument aligns its internal gains to the 50 MHz Amplitude Reference.

b. Absolute Amplitude Accuracy for a wide range of signal and measurement settings, covers the 95th percentile proportion with 95% confidence. Here are the details of what is covered and how the computation is made:

The wide range of conditions of RBW, signal level, VBW, reference level and display scale are discussed in footnote a. There are 108 quasi-random combinations used, tested at a 50 MHz signal frequency. We compute the 95th percentile proportion with 95% confidence for this set observed over a statistically significant number of instruments. Also, the frequency response relative to the 50 MHz response is characterized by varying the signal across a large number of quasi-random verification frequencies that are chosen to not correspond with the frequency response adjustment frequencies. We again compute the 95th percentile proportion with 95% confidence for this set observed over a statistically significant number of instruments. We also compute the 95th percentile accuracy of tracing the calibration of the 50 MHz absolute amplitude accuracy to a national standards organization. We also compute the 95th percentile accuracy of tracing the calibration of the relative frequency response to a national standards organization. We take the root-sum-square of these four independent Gaussian parameters. To that rss we add the environmental effects of temperature variations across the 20 to 30°C range.

c. Same settings as footnote a, except that the signal level at the preamp input is -40 to -80 dBm. Total power at preamp (dBm) = total power at input (dBm) minus input attenuation (dB). This specification applies for signal frequencies above 100 kHz.

a. The nominal SWR stated is given for the worst case RF frequency in three representative instruments.

Keysight CXA Signal Analyzer Amplitude Accuracy and Range

a. Because reference level affects only the display, not the measurement, it causes no additional error in measurement results from trace data or markers.

a. Because Log/Lin and Log Scale Switching affect only the display, not the measurement, they cause no additional error in measurement results from trace data or markers.

a. Supplemental information: The amplitude detection linearity specification applies at all levels below -10 dBm at the input mixer; however, noise will reduce the accuracy of low level measurements. The amplitude error due to noise is determined by the signal-to-noise ratio, S/N. If the S/N is large (20 dB or better), the amplitude error due to noise can be estimated from the equation below, given for the 3-sigma (three standard deviations) level.

$$
3\sigma = 3(20dB)\log(1 + 10^{-((S/N + 3dB)/20dB)})
$$

T

he errors due to S/N ratio can be further reduced by averaging results. For large S/N (20 dB or better), the 3-sigma level can be reduced proportional to the square root of the number of averages taken.

- b. The scale fidelity is warranted with ADC dither set to Medium. Dither increases the noise level by nominally only 0.24 dB for the most sensitive case (preamp Off, best DANL frequencies). With dither Off, scale fidelity for low level signals, around -60 dBm or lower, will nominally degrade by 0.2 dB.
- c. Reference level and off-screen performance: The reference level (RL) behavior differs from some earlier analyzers in a way that makes this analyzer more flexible. In other analyzers, the RL controlled how the measurement was performed as well as how it was displayed. Because the logarithmic amplifier in these analyzers had both range and resolution limitations, this behavior was necessary for optimum measurement accuracy. The logarithmic amplifier in this signal analyzer, however, is implemented digitally such that the range and resolution greatly exceed other instrument limitations. Because of this, the analyzer can make measurements largely independent of the setting of the RL without compromising accuracy. Because the RL becomes a display function, not a measurement function, a marker can read out results that are off-screen, either above or below, without any change in accuracy. The only exception to the independence of RL and the way in which the measurement is performed is in the input attenuator setting: When the input attenuator is set to auto, the rules for the determination of the input attenuation include dependence on the reference level. Because the input attenuation setting controls the tradeoff between large signal behaviors (third-order intermodulation and compression) and small signal effects (noise), the measurement results can change with RL changes when the input attenuation is set to auto.
- d. Mixer level = Input Level Input Attenuator
- e. The relative fidelity is the error in the measured difference between two signal levels. It is so small in many cases that it cannot be verified without being dominated by measurement uncertainty of the verification. Because of this verification difficulty, this specification gives nominal performance, based on numbers that are as conservatively determined as those used in warranted specifications. We will consider one example of the use of the error equation to compute the nominal performance. Example: the accuracy of the relative level of a sideband around -60 dBm, with a carrier at -5 dBm, using attenuator = 10 dB, RBW = 3 kHz, evaluated with swept analysis. The high level term is evaluated with $P1 = -15$ dBm and $P2 = -70$ dBm at the mixer. This gives a maximum error within ± 0.025 dB. The instability term is ± 0.018 dB. The slope term evaluates to ± 0.050 dB. The sum of all these terms is ± 0.093 dB.
- f. Errors at high mixer levels will nominally be well within the range of ± 0.045 dB \times {exp[(P1 $-$ Pref)/(8.69 dB)] $-$ exp[(P2 $-$ Pref)/(8.69 dB)]}. In this expression, P1 and P2 are the powers of the two signals, in decibel units, whose relative power is being measured. Pref is -10 dBm. All these levels are referred to the mixer level.
- g. Slope error will nominally be well within the range of $\pm 0.0009 \times (P1 P2)$. P1 and P2 are defined in footnote [f.](#page-26-6)

Dynamic Range

Gain Compression

a. Large signals, even at frequencies not shown on the screen, can cause the analyzer to incorrectly measure on-screen signals because of two-tone gain compression. This specification tells how large an interfering signal must be in order to cause a 1 dB change in an on-screen signal.

b. Specified at 1 kHz RBW with 1 MHz tone spacing.

c. Reference level and off-screen performance: The reference level (RL) behavior differs from some earlier analyzers in a way that makes this analyzer more flexible. In other analyzers, the RL controlled how the measurement was performed as well as how it was displayed. Because the logarithmic amplifier in these analyzers had both range and resolution limitations, this behavior was necessary for optimum measurement accuracy. The logarithmic amplifier in this signal analyzer, however, is implemented digitally such that the range and resolution greatly exceed other instrument limitations. Because of this, the analyzer can make measurements largely independent of the setting of the RL without compromising accuracy. Because the RL becomes a display function, not a measurement function, a marker can read out results that are off-screen, either above or below, without any change in accuracy. The only exception to the independence of RL and the way in which the measurement is performed is in the input attenuation setting: When the input attenuation is set to auto, the rules for the determination of the input attenuation include dependence on the reference level. Because the input attenuation setting controls the tradeoff between large signal behaviors (third-order intermodulation, compression, and display scale fidelity) and small signal effects (noise), the measurement results can change with RL changes when the input attenuation is set to auto.

d. Mixer power level (dBm) = input power (dBm) – input attenuation (dB) .

Displayed Average Noise Level

a. DANL for zero span and swept is measured in a 1 kHz RBW and normalized to the narrowest available RBW, because the noise figure does not depend on RBW and 1 kHz measurements are faster.

b. DANL below 10 MHz is affected by phase noise around the LO feedthrough signal.

c. DANL below 10 MHz is affected by phase noise around the LO feedthrough signal. Specifications apply with the best setting of the Phase Noise Optimization control, which is to choose the "Best Close-in f Noise" for frequencies below 25 kHz, and "Best Wide Offset f Noise" for frequencies above 85 kHz.

Spurious Response

a. Mixer Level = Input Level - Input Attenuation.

b. The spurious response specifications only apply with the preamp turned off. When the preamp is turned on, performance is nominally the same as long as the mixer level is interpreted to be: Mixer Level = Input Level – Input Attenuation – Preamp Gain.

c. Input terminated, 0 dB input attenuation.

d. The stop frequency varies according to the option 503/507/513/526 selected.

Second Harmonic Distortion

a. SHI = second harmonic intercept. The SHI is given by the mixer power in dBm minus the second harmonic distortion level relative to the mixer tone in dBc.

Third Order Intermodulation

a. TOI is verified with IF Gain set to its best case condition, which is IF Gain = Low.

b. Intercept = TOI = third order intercept. The TOI is given by the mixer tone level (in dBm) minus (distortion/2) where distortion is the relative level of the distortion tones in dBc.

c. The distortion shown is computed from the warranted intercept specifications, based on two tones at –20 dBm each, instead of being measured directly.

Phase Noise

a. The nominal performance of the phase noise at center frequencies different than the one at which the specifications apply (1 GHz) depends on the center frequency, band and the offset. For low offset frequencies, offsets well under 100 Hz, the phase noise increases by $20 \times \log[(f + 0.3225)/1.3225]$. For mid-offset frequencies such as 10 kHz, band 0 phase noise increases as $20 \times \log[(f + 5.1225)/6.1225]$. For mid-offset frequencies in other bands, phase noise changes as $20 \times \log[(f + 0.3225)/6.1225]$ except f in this expression should never be lower than 5.8. For wide offset frequencies, offsets above about 100 kHz, phase noise increases as $20 \times \log(N)$. N is the LO Multiple as shown on [page 11](#page-10-2); f is in GHz units in all these relationships; all increases are in units of decibels.

b. Noise sidebands for lower offset frequencies, for example, 10 kHz, apply with the phase noise optimization (**PhNoise Opt**) set to **Best Close-in Noise**. Noise sidebands for higher offset frequencies, for example, 1 MHz, as shown apply with the phase noise optimization set to **Best Wide-offset** ϕ **Noise**.

c. Specifications are given with the internal frequency reference. The phase noise at offsets below 100 Hz is impacted or dominated by noise from the reference. Thus, performance with external references will not follow the curves and specifications. The internal 10 MHz reference phase noise is about –120 dBc/Hz at 10 Hz offset; external references with poorer phase noise than this will cause poorer performance than shown.

Power Suite Measurements

a. See ["Absolute Amplitude Accuracy" on page 23](#page-22-3).

b. See ["Power Bandwidth Accuracy" on page 18](#page-17-2).

c. Expressed in dB.

a. The effect of scale fidelity on the ratio of two powers is called the relative scale fidelity. The scale fidelity specified in the Amplitude section is an absolute scale fidelity with -35 dBm at the input mixer as the reference point. The relative scale fidelity is nominally only 0.01 dB larger than the absolute scale fidelity.

b. See Amplitude Accuracy and Range section.

c. See Frequency and Time section.

d. Expressed in decibels.

Keysight CXA Signal Analyzer Power Suite Measurements

- e. An ACP measurement measures the power in adjacent channels. The shape of the response versus frequency of those adjacent channels is occasionally critical. One parameter of the shape is its 3 dB bandwidth. When the bandwidth (called the Ref BW) of the adjacent channel is set, it is the 3 dB bandwidth that is set. The passband response is given by the convolution of two functions: a rectangle of width equal to Ref BW and the power response versus frequency of the RBW filter used. Measurements and specifications of analog radio ACPs are often based on defined bandwidths of measuring receivers, and these are defined by their -6 dB widths, not their -3 dB widths. To achieve a passband whose -6 dB width is x, set the Ref BW to be $x-0.572 \times \mathrm{RBW}$.
- f. Most versions of adjacent channel power measurements use negative numbers, in units of dBc, to refer to the power in an adjacent channel relative to the power in a main channel, in accordance with ITU standards. The standards for W-CDMA analysis include ACLR, a positive number represented in dB units. In order to be consistent with other kinds of ACP measurements, this measurement and its specifications will use negative dBc results, and refer to them as ACPR, instead of positive dB results referred to as ACLR. The ACLR can be determined from the ACPR reported by merely reversing the sign.
- g. The accuracy of the Adjacent Channel Power Ratio will depend on the mixer drive level and whether the distortion products from the analyzer are coherent with those in the UUT. These specifications apply even in the worst case condition of coherent analyzer and UUT distortion products. For ACPR levels other than those in this specifications table, the optimum mixer drive level for accuracy is approximately -37 dBm $-$ (ACPR/3), where the ACPR is given in (negative) decibels.
- h. The Fast method has a slight decrease in accuracy in only one case: for BTS measurements at 5 MHz offset, the accuracy degrades by ± 0.01 dB relative to the accuracy shown in this table.
- i. To meet this specified accuracy when measuring mobile station (MS) or user equipment (UE) within 3 dB of the required -33 dBc ACPR, the mixer level (ML) must be optimized for accuracy. This optimum mixer level is -20 dBm, so the input attenuation must be set as close as possible to the average input power (-20 dBm) . For example, if the average input power is -6 dBm, set the attenuation to 14 dB. This specification applies for the normal 3.5 dB peak-to-average ratio of a single code. Note that if the mixer level is set to optimize dynamic range instead of accuracy, accuracy errors are nominally doubled.
- ACPR accuracy at 10 MHz offset is warranted when the input attenuator is set to give an average mixer level of -10 dBm.
- k. In order to meet this specified accuracy, the mixer level must be optimized for accuracy when measuring node B Base Transmission Station (BTS) within 3 dB of the required -45 dBc ACPR. This optimum mixer level is -18 dBm, so the input attenuation must be set as close as possible to the average input power $-(-18$ dBm). For example, if the average input power is -5 dBm, set the attenuation to 13 dB. This specification applies for the normal 10 dB peak-to-average ratio (at 0.01% probability) for Test Model 1. Note that, if the mixer level is set to optimize dynamic range instead of accuracy, accuracy errors are nominally doubled.
- l. Accuracy can be excellent even at low ACPR levels assuming that the user sets the mixer level to optimize the dynamic range, and assuming that the analyzer and UUT distortions are incoherent. When the errors from the UUT and the analyzer are incoherent, optimizing dynamic range is equivalent to minimizing the contribution of analyzer noise and distortion to accuracy, though the higher mixer level increases the display scale fidelity errors. This incoherent addition case is commonly used in the industry and can be useful for comparison of analysis equipment, but this incoherent addition model is rarely justified. This derived accuracy specification is based on a mixer level of -13 dBm.
- m. Keysight measures 100% of the signal analyzers for dynamic range in the factory production process. This measurement requires a near-ideal signal, which is impractical for field and customer use. Because field verification is impractical, Keysight only gives a typical result. More than 80% of prototype instruments met this "typical" specification; the factory test line limit is set commensurate with an on-going 80% yield to this typical.

The ACPR dynamic range is verified only at 2 GHz, where Keysight has the near-perfect signal available. The dynamic range is specified for the optimum mixer drive level, which is different in different instruments and different conditions. The test signal is a 1 DPCH signal.

The ACPR dynamic range is the observed range. This typical specification includes no measurement uncertainty.

a. The RBW method measures the power in the adjacent channels within the defined resolution bandwidth. The noise bandwidth of the RBW filter is nominally 1.055 times the 3.01 dB bandwidth. Therefore, the RBW method will nominally read 0.23 dB higher adjacent channel power than would a measurement using the integration bandwidth method, because the noise bandwidth of the integration bandwidth measurement is equal to that integration bandwidth. For cdmaOne ACPR measurements using the RBW method, the main channel is measured in a 3 MHz RBW, which does not respond to all the power in the carrier. Therefore, the carrier power is compensated by the expected under-response of the filter to a full width signal, of 0.15 dB. But the adjacent channel power is not compensated for the noise bandwidth effect.

The reason the adjacent channel is not compensated is subtle. The RBW method of measuring ACPR is very similar to the preferred method of making measurements for compliance with FCC requirements, the source of the specifications for the cdmaOne Spur Close specifications. ACPR is a spot measurement of Spur Close, and thus is best done with the RBW method, even though the results will disagree by 0.23 dB from the measurement made with a rectangular passband.

b. The specified ACPR accuracy applies if the measured ACPR substantially exceeds the analyzer dynamic range at the specified offset. When this condition is not met, there are additional errors due to the addition of analyzer spectral components to UUT spectral components. In the worst case at these offsets, the analyzer spectral components are all coherent with the UUT components; in a more typical case, one third of the analyzer spectral power will be coherent with the distortion components in the UUT. Coherent means that the phases of the UUT distortion components and the analyzer distortion components are in a fixed relationship, and could be perfectly in-phase. This coherence is not intuitive to many users, because the signals themselves are usually pseudo-random; nonetheless, they can be coherent.

When the analyzer components are 100% coherent with the UUT components, the errors add in a voltage sense. That error is a function of the signal (UUT ACPR) to noise (analyzer ACPR dynamic range limitation) ratio, SN, in decibels.

The function is error = $20 \times \log(1 + 10^{-5N/20})$

For example, if the UUT ACPR is -62 dB and the measurement floor is -82 dB, the SN is 20 dB and the error due to adding the analyzer distortion to that of the UUT is 0.83 dB.

c. As in footnote [b,](#page-38-0) the specified ACPR accuracy applies if the ACPR measured substantially exceeds the analyzer dynamic range at the specified offset. When this condition is not met, there are additional errors due to the addition of analyzer spectral components to UUT spectral components. Unlike the situation in footnote [b](#page-38-0), though, the spectral components from the analyzer will be non-coherent with the components from the UUT. Therefore, the errors add in a power sense. The error is a function of the signal (UUT ACPR) to noise (analyzer ACPR dynamic range limitation) ratio, SN, in decibels.

The function is error = $10 \times \log(1 + 10^{-SN/10})$.

For example, if the UUT ACPR is -75 dB and the measurement floor is -85 dB, the SN ratio is 10 dB and the error due to adding the analyzer's noise to that of the UUT is 0.41 dB.

a. The Complementary Cumulative Distribution Function (CCDF) is a reformatting of a histogram of the power envelope. The width of the amplitude bins used by the histogram is the histogram resolution. The resolution of the CCDF will be the same as the width of those bins.

a. The dynamic is specified at 12.5 MHz offset from center frequency with the mixer level of 1 dB of compression point, which will degrade accuracy 1 dB.

b. The sensitivity is specified at far offset from carrier, where phase noise does not contribute. You can derive the dynamic range at far offset 1 dB compression mixer level and sensitivity.

a. The dynamic range specification is the ratio of the channel power to the power in the offset specified. The dynamic range depends on the measurement settings, such as peak power or integrated power. Dynamic range specifications are based on default measurement settings, with detector set to average, and depend on the mixer level. Default measurement settings include 30 kHz RBW.

b. This dynamic range specification applies for the optimum mixer level, which is about -16 dBm. Mixer level is defined to be the average input power minus the input attenuation.

c. The sensitivity is specified with 0 dB input attenuation. It represents the noise limitations of the analyzer. It is tested without an input signal. The sensitivity at this offset is specified in the default 30 kHz RBW, at a center frequency of 2 GHz.

d. The relative accuracy is a measure of the ratio of the power at the offset to the main channel power. It applies for spectrum emission levels in the offset s that are well above the dynamic range limitation.

e. The absolute accuracy of SEM measurement is the same as the absolute accuracy of the spectrum analyzer. See ["Amplitude](#page-19-0) [Accuracy and Range" on page 20](#page-19-0) for more information. The numbers shown are for 0 to 3.0 GHz, with attenuation set to 10 dB.

Options

The following options and applications affect instrument specifications.

General

a. The LCD display is manufactured using high precision technology. However, there may be up to six bright points (white, blue, red or green in color) that constantly appear on the LCD screen. These points are normal in the manufacturing process and do not affect the measurement integrity of the product in any way.

a. Sweep Points = 101

b. Factory preset, fixed center frequency, RBW = 1 MHz, and span > 10 MHz and \leq 600 MHz, Auto Align Off.

c. Phase Noise Optimization set to Fast Tuning, Display Off, 32 bit integer format, markers Off, single sweep, Keysight I/O Libraries Suite Version 14.1, one meter GPIB cable, National Instruments PCI-GPIB Card and NI-488.2 DLL.

Inputs/Outputs

Front Panel

Keysight CXA Signal Analyzer Inputs/Outputs

Rear Panel

Regulatory Information

This product is designed for use in Installation Category II and Pollution Degree 2 per IEC 61010 2nd ed, and 664 respectively.

This product has been designed and tested in accordance with accepted industry standards, and has been supplied in a safe condition. The instruction documentation contains information and warnings which must be followed by the user to ensure safe operation and to maintain the product in a safe condition.

Keysight CXA Signal Analyzer Declaration of Conformity

Declaration of Conformity

A copy of the Manufacturer's European Declaration of Conformity for this instrument can be obtained by contacting your local Keysight Technologies sales representative.

I/Q Analyzer

Specification Guide

This chapter contains specifications for the I/Q Analyzer measurement application (Basic Mode).

Specifications Affected by I/Q Analyzer

Frequency

Clipping-to-Noise Dynamic Range

a. This specification is defined to be the ratio of the clipping level (also known as "ADC Over Range") to the noise density. In decibel units, it can be defined as clipping level $[dBm]$ – noise density $[dBm/Hz]$; the result has units of dBfs/Hz (fs is "full scale").

b. The noise density depends on the input frequency. It is lowest for a broad range of input frequencies near the center frequency, and these specifications apply there. The noise density can increase toward the edges of the span. The effect is nominally well under 1 dB.

c. The primary determining element in the noise density is the ["Displayed Average Noise Level" on page 30](#page-29-0).

d. DANL is specified for log averaging, not power averaging, and thus is 2.51 dB lower than the true noise density. It is also specified in the narrowest RBW, 1 Hz, which has a noise bandwidth slightly wider than 1 Hz. These two effects together add up to 2.25 dB.

Data Acquisition

I/Q Analyzer Data Acquisition Specification Guide

3 Option CR3 - Connector Rear, Second IF Output

This chapter contains specifications for the CXA Signal Analyzer Option CR3, Second IF Output.

This option is only available for Frequency Option 503 or 507.

Specifications Affected by Connector Rear, Second IF Output

No other analyzer specifications are affected by the presence or use of this option. New specifications are given in the following page.

Other Connector Rear, Second IF Output Specifications

Second IF Out Port

Second IF Out

a. "Conversion Gain" is defined from RF input to IF Output with 0 dB attenuation. The nominal performance applies with zero span.

b. Measured from 262.5 to 382.5 MHz for low band or 302.5 to 342.5 MHz for high band.

Option CR3 - Connector Rear, Second IF Output Other Connector Rear, Second IF Output Specifications Specification Guide

4 Option C75 - Connector Front, 75 Ohm Additional RF Input, 1.5 GHz

This chapter contains the specifications for Option C75, Connector Front, 75 Ω Additional RF Input, 1.5 GHz.

This option is only available for Frequency Option 503 or 507.

Specifications Affected by Connector, 75Ohm Additional RF Input, 1.5 GHz

a. SHI = second harmonic intercept. The SHI is given by the mixer power in dBm minus the second harmonic distortion level relative to the mixer tone in dBc.

a. The nominal SWR stated is given for the worst case RF frequency in three representative instruments.

Option C75 - Connector Front, 75 Ohm Additional RF Input, 1.5 GHz Specifications Affected by Connector, 75 Ohm Additional RF Input, 1.5 GHz

- a. Large signals, even at frequencies not shown on the screen, can cause the analyzer to incorrectly measure on-screen signals because of two-tone gain compression. This specification tells how large an interfering signal must be in order to cause a 1 dB change in an on-screen signal.
- b. Specified at 1 kHz RBW with 1 MHz tone spacing.
- c. Reference level and off-screen performance: The reference level (RL) behavior differs from some earlier analyzers in a way that makes this analyzer more flexible. In other analyzers, the RL controlled how the measurement was performed as well as how it was displayed. Because the logarithmic amplifier in these analyzers had both range and resolution limitations, this behavior was necessary for optimum measurement accuracy. The logarithmic amplifier in this signal analyzer, however, is implemented digitally such that the range and resolution greatly exceed other instrument limitations. Because of this, the analyzer can make measurements largely independent of the setting of the RL without compromising accuracy. Because the RL becomes a display function, not a measurement function, a marker can read out results that are off-screen, either above or below, without any change in accuracy. The only exception to the independence of RL and the way in which the measurement is performed is in the input attenuation setting: When the input attenuation is set to auto, the rules for the determination of the input attenuation include dependence on the reference level. Because the input attenuation setting controls the tradeoff between large signal behaviors (third-order intermodulation, compression, and display scale fidelity) and small signal effects (noise), the measurement results can change with RL changes when the input attenuation is set to auto.
- d. Mixer power level (dBm) = input power (dBm) input attenuation (dB) .

a. DANL for zero span and swept is normalized in two ways and for two reasons. DANL is measured in a 1 kHz RBW and normalized to the narrowest available RBW, because the noise figure does not depend on RBW and 1 kHz measurements are faster. The second normalization is that DANL is measured with 10 dB input attenuation and normalized to the 0 dB input attenuation case, because that makes DANL and third order intermodulation test conditions congruent, allowing accurate dynamic range estimation for the analyzer.

Other Connector, 75 Ohm Additional RF Input, 1.5 GHz Specifications

Specification Guide

5 Option EMC - Precompliance EMI Features

This chapter contains specifications for the *Option EMC* precompliance EMI feature.

Frequency

Table 5-1 CISPR Band Settings

Table 5-2 MIL-STD 461D/E/F Frequency Ranges and Bandwidths

Amplitude

Option EMC - Precompliance EMI Features Amplitude
Specification Guide

6 Option B25 (25 MHz) - Analysis Bandwidth

This chapter contains specifications for the Option B25 (25 MHz) Analysis Bandwidth, and are unique to this IF Path.

Specifications Affected by Analysis Bandwidth

The specifications in this chapter apply when the 25 MHz path is in use. In IQ Analyzer, this will occur when the IF Path is set to 25 MHz, whether by Auto selection (depending on Span) or manually.

Other Analysis Bandwidth Specifications

a. To save test time, the levels of these spurs are not warranted. However, the relationship between the spurious response and its excitation is described so the user can distinguish whether a questionable response is due to these mechanisms or is subject to the specifications in "Spurious Responses" in the core specifications. f is the apparent frequency of the spurious, fc is the measurement center frequency.

b. The spurious response specifications only apply with the preamp turned off. When the preamp is turned on, performance is nominally the same as long as the mixer level is interpreted to be Mixer Level = Input Level - Input Attenuation - Preamp Gain

c. Mixer Level = Input Level - Input Attenuation.

Option B25 (25 MHz) - Analysis Bandwidth Other Analysis Bandwidth Specifications

a. The IF frequency response includes effects due to RF circuits such as input filters, that are a function of RF frequency, in addition to the IF pass-band effects.

b. Signal frequencies between 18 and 26.5 GHz are prone to additional response errors due to modes in the Type-N connector used with frequency Option 526. With the use of Type-N to APC 3.5 mm adapter part number 1250-1744, there are nominally six such modes. These modes cause nominally up to –0.35 dB amplitude change, with phase errors of nominally up to $\pm 1.2^{\circ}$.

- c. The maximum error at an offset (f) from the center of the FFT width is given by the expression \pm [Midwidth Error + (f \times Slope)], but never exceeds \pm Max Error. Usually, the span is no larger than the FFT width in which case the center of the FFT width is the center frequency of the analyzer. When the analyzer span is wider than the FFT width, the span is made up of multiple concatenated FFT results, and thus has multiple centers of FFT widths so the f in the equation is the offset from the nearest center. These specifications include the effect of RF frequency response as well as IF frequency response at the worst case center frequency. Performance is nominally three times better than the maximum error at most center frequencies.
- d. The specification does not apply for frequencies greater than 3.6 MHz from the center in FFT Widths of 7.2 to 8 MHz.
- e. The "RMS" nominal performance is the standard deviation of the response relative to the center frequency, integrated across a 10 MHz span. This performance measure was observed at a single center frequency in each harmonic mixing band, which is representative of all center frequencies; the observation center frequency is not the worst case center frequency.

a. Signal frequencies between 18 and 26.5 GHz are prone to additional response errors due to modes in the Type-N connector used with frequency Option 526. With the use of Type-N to APC 3.5 mm adapter part number 1250-1744, there are nominally six such modes. These modes cause nominally up to -0.35 dB amplitude change, with phase errors of nominally up to $\pm 1.2^{\circ}$.

b. The listed performance is the standard deviation of the phase deviation relative to the mean phase deviation from a linear phase condition, where the RMS is computed across the span shown.

a. This table is meant to help predict the full-scale level, defined as the signal level for which ADC overload (clipping) occurs. The prediction is imperfect, but can serve as a starting point for finding that level experimentally. A SCPI command is also available for that purpose.

b. Mixer level is signal level minus input attenuation.

c. The available gain to reach the predicted mixer level will vary with center frequency. Combinations of high gains and high frequencies will not achieve the gain required, increasing the full scale level.

Data Acquisition

Specification Guide

7 Option P03, P07, P13 and P26 - Preamplifiers

This chapter contains specifications for the CXA Signal Analyzer *Options P03, P07, P13* and *P26* preamplifiers.

Specifications Affected by Preamp

Other Preamp Specifications

a. Nominally, the noise figure of the spectrum analyzer is given by

 $NF = D$. $(K L + N + B)$

where, D is the DANL (displayed average noise level) specification (Refer to [page 83](#page-82-0) for DANL with Preamp),

K is kTB (.173.98 dBm in a 1 Hz bandwidth at 290 K),

L is 2.51 dB (the effect of log averaging used in DANL verifications)

N is 0.24 dB (the ratio of the noise bandwidth of the RBW filter with which DANL is specified to an ideal noise bandwidth) B is ten times the base-10 logarithm of the RBW (in hertz) in which the DANL is specified. B is 0 dB for the 1 Hz RBW. The actual NF will vary from the nominal due to frequency response errors.

b. The effect of AC coupling is negligible for frequencies above 40 MHz. Below 40 MHz, DC coupling is recommended for the best measurements. The instrument NF nominally degrades by 0.2 dB at 30 MHz and 1 dB at 10 MHz with AC coupling.

a. Large signals, even at frequencies not shown on the screen, can cause the analyzer to incorrectly measure on-screen signals because of two-tone gain compression. This specification tells how large an interfering signal must be in order to cause a 1 dB change in an on-screen signal.

b. Specified at 1 kHz RBW with 1 MHz tone spacing.

c. Reference level and off-screen performance: The reference level (RL) behavior differs from some earlier analyzers in a way that makes this analyzer more flexible. In other analyzers, the RL controlled how the measurement was performed as well as how it was displayed. Because the logarithmic amplifier in these analyzers had both range and resolution limitations, this behavior was necessary for optimum measurement accuracy. The logarithmic amplifier in this signal analyzer, however, is implemented digitally such that the range and resolution greatly exceed other instrument limitations. Because of this, the analyzer can make measurements largely independent of the setting of the RL without compromising accuracy. Because the RL becomes a display function, not a measurement function, a marker can read out results that are off-screen, either above or below, without any change in accuracy. The only exception to the independence of RL and the way in which the measurement is performed is in the input attenuation setting: When the input attenuation is set to auto, the rules for the determination of the input attenuation include dependence on the reference level. Because the input attenuation setting controls the tradeoff between large signal behaviors (third-order intermodulation, compression, and display scale fidelity) and small signal effects (noise), the measurement results can change with RL changes when the input attenuation is set to auto.

d. Total power at the preamp (dBm) = total powr at the input (dBm) - input attenuation (dB).

a. DANL for zero span and swept is measured in a 1 kHz RBW and normalized to the narrowest available RBW, because the noise figure does not depend on RBW and 1 kHz measurements are faster. Specificatons for 10 MHz to 3 GHz apply with AC coupled.

b. DANL below 10 MHz is affected by phase noise around the LO feedthrough signal.

c. DANL below 10 MHz is affected by phase noise around the LO feedthrough signal. Specifications apply with the best setting of the Phase Noise Optimization control, which is to choose the "Best Close-in f Noise" for frequencies below 25 kHz, and "Best Wide Offset f Noise" for frequencies above 85 kHz.

a. For Sweep Type = FFT, add the RF flatness errors of this table to the IF Frequency Response errors. An additional error source, the error in switching between swept and FFT sweep types, is nominally ±0.01 dB and is included within the "Absolute Amplitude Error" specifications.

Option P03, P07, P13 and P26 - Preamplifiers Other Preamp Specifications

Specification Guide

8 Options T03 and T06 - Tracking Generators

This chapter contains specifications for the CXA Signal Analyzer *Option T03* and *T06* tracking generators.

This option is only available for Frequency *Option 503* or *507*.

General Specifications

a. The nominal performance of the phase noise at frequencies above the frequency at which the specifications apply (1 GHz) depends on the band and the offset.

b. Specifications are given with the internal frequency reference.

a. Center Frequency = 1 GHz, RBW = 1 kHz, 10 dB attenuation.

Specification Guide

9 Option ESC - External Source Control

This chapter contains specifications for the *Option ESC*, External Source Control.

This option is only avaiable for Frequency *Option 503* or *507*.

Frequency

a. Limited by the frequency range of the source to be controlled.

b. The analyzer always sweeps in a positive direction, but the source may be configured to sweep in the opposite direction. This can be useful for analyzing negative mixing products in a mixer under test, for example.

a. The dynamic range is given by this computation: –10 dBm – DANL – 10×log(RBW) where DANL is the displayed average noise level specification, normalized to 1 Hz RBW, and the RBW used in the measurement is in hertz units. The dynamic range can be increased by reducing the RBW at the expense of increased sweep time.

b. The following footnotes discuss the biggest contributors to amplitude accuracy.

c. One amplitude accuracy contributor is the linearity with which amplitude levels are detected by the analyzer. This is called "scale fidelity" by most spectrum analyzer users, and "dynamic amplitude accuracy" by most network analyzer users. This small term is documented in the Amplitude section of the Specifications Guide. It is negligibly small in most cases.

- d. The amplitude accuracy versus frequency in the source and the analyzer can contribute to amplitude errors. This error source is eliminated when using normalization.
- e. VSWR interaction effects, caused by RF reflections due to mismatches in impedance, are usually the dominant error source. These reflections can be minimized by using 10 dB or more attenuation in the analyzer, and using well-matched attenuators in the measurement configuration.

a. Relative to the original power level and limited by the source to be controlled.

Option ESC - External Source Control Frequency

a. These measurement times were observed with a span of 100 MHz, RBW of 20 kHz and the point triggering method being set to EXT TRIG1. The measurement times will not change significantly with span when the RBW is automatically selected. If the RBW is decreased, the sweep time increase would be approximately 23.8 times Npoints/RBW.

b. Based on MXG firmware version A.01.51.

Specification Guide

10 Options PFR - Precision Frequency Reference

This chapter contains specifications for the *Option PFR* Precision Frequency Reference.

Specifications Affected by Precision Frequency Reference

Specification Guide

11 Analog Demodulation Measurement Application

This chapter contains specifications for the N9063C Analog Demodulation Measurement Application.

Additional Definitions and Requirements

The warranted specifications shown apply to Band 0 operation (up to 3.0 GHz), unless otherwise noted, for all analyzer's. The application functions, with nominal (non-warranted) performance, at any frequency within the frequency range set by the analyzer frequency options (see table). In practice, the lowest and highest frequency of operation may be further limited by AC coupling; by "folding" near 0 Hz; by DC feedthrough; and by Channel BW needed. Phase noise and residual FM generally increase in higher bands.

Warranted specifications shown apply when Channel BW \leq 1 MHz, unless otherwise noted. (Channel BW is an important user-settable control.) The application functions, with nominal (non-warranted) performance, at any Channel BW up to the analyzer's bandwidth options (see table). The Channel BW required for a measurement depends on: the type of modulation (AM, FM, PM); the rate of modulation; the modulation depth or deviation; and the spectral contents (e.g. harmonics) of the modulating tone.

Many specs require that the Channel BW control is optimized; neither too narrow nor too wide.

Many warranted specifications (rate, distortion) apply only in the case of a single, sinusoidal modulating tone; without excessive harmonics, non-harmonics, spurs, or noise. Harmonics, which are included in most distortion results, are counted up to the 10th harmonic of the dominant tone, or as limited by SINAD BW or post-demod filters. Note that SINAD will include Carrier Frequency Error (the "DC term") in FM by default; it can be eliminated with a HPF or Auto Carrier Frequency feature.

Warranted specifications apply to results of the software application; the hardware demodulator driving the Analog Out line is described separately.

Warranted specifications apply over an operating temperature range of 20 to 30 °C; and mixer level –24 to –18 dBm (mixer level = Input power level – Attenuation). Additional conditions are listed at the beginning of the FM, AM, and PM sections, in specification tables, or in footnotes.

Refer to the footnote for ["Definitions of terms used in this chapter" on page 98](#page-97-0).

Definitions of terms used in this chapter

Let $P_{signal}(S)$ = Power of the signal; $P_{noise}(N)$ =Power of the noise; $P_{distortion}(D)$ = Power of the harmonic distortion (P_{H2} +P_{H3} + ... + P_{Hi} where H_i is the ith harmonic that counts up to the 10th harmonic); P_{total} = Total power of the signal, noise and distortion components.

NOTE P_{Noise} must be limited to the bandwidth of the applied filters. The harmonic sequence is limited to the 10th harmonic unless otherwise indicated. In practice, the term P_{noise} includes Spurs, IMD, Hum, etc. (All but harmonics.)

RF Carrier Frequency and Bandwidth

a. The maximum InfoBW indicates the maximum operational BW, which depends on the analysis BW option equipped with the analyzer. However, the demodulation specifications only apply to the BW indicated in the following sections.

b. Sample rate is set indirectly by the user, with the Span and Channel BW controls (viewed in RF Spec- trum). The Info BW (also called Demodulation BW) is based on the larger of the two; specifically, InfoBW = max [Span, Channel BW]. The sample interval is $1/(1.25 \times$ Info BW); e.g. if InfoBW = 200 kHz, then sample interval is 4 us. The sample rate is $1.25 \times$ InfoBW, or $1.25 \times$ max [Span, Channel BW]. These values are approximate, to estimate memory usage. Exact values can be queried via SCPI while the application is running.

Demod Time is a user setting. Generally, it should be 3- to 5-times the period of the lowest-frequency modulating tone.

Post-Demodulation

a. ITU standards specify that CCIR-1k Weighted and CCIR Unweighted filters use Quasi-Peak-Detection (QPD). However, the implementation in N9063C is based on true-RMS detection, scaled to respond as QPD. The approximation is valid when measuring amplitude of Gaussian noise, or SINAD of a single continuous sine tone (e.g. 1 kHz), with harmonics, combined with Gaussian noise. The results may not be consistent with QPD if the input signal is bursty, clicky, or impulsive; or contains non-harmonically related tones (multi-tone, intermods, spurs) above the noise level. Use the AF Spectrum trace to vali- date these assumptions. Consider using Keysight U8903A Audio Analyzer if true QPD is required.

Frequency Modulation

Conditions required to meet specification

- Peak deviation^{*}: **≥** 200 Hz
- Modulation index (ModIndex) =PeakDeviation/Rate = Beta: 0.2 to 2000
- Channel BW: \leq 50 kHz
- Rate: 20 Hz to 50 kHz
- SINAD bandwidth: (Channel BW) / 2
- Single tone sinusoid modulation

- a. This specification applies to the result labeled "(Pk-Pk)/2".
- b. For optimum measurement of rate and deviation, ensure that the channel bandwidth is set wide enough to capture the significant RF energy (as visible in the RF Spectrum window). Setting the channel bandwidth too wide will result in measurement errors.
- c. Reading is a measured frequency peak deviation in Hz, and Rate is a modulation rate in Hz.
- d. Reading is a measured modulation rate in Hz.

^{*.}Peak deviation, modulation index ("beta"), and modulation rate are related by PeakDeviation = ModIndex Rate. Each of these has an allowable range, but all conditions must be satisfied at the same time. For example, PeakDeviation = 80 kHz at Rate = 20 Hz is not allowed, since ModIndex = PeakDeviation/Rate would be 4000, but ModIndex is limited to 2000. In addition, all significant sidebands must be contained in Channel BW. For FM, an approximate rule-of-thumb is $2 \times$ [PeakDeviation + Rate] < Channel BW; this implies that PeakDeviation might be large if the Rate is small, but both cannot be large at the same time.

Frequency Modulation

a. For optimum measurement, ensure that the Channel BW is set wide enough to capture the significant RF energy. Setting the Channel BW too wide will result in measurement errors.

b. SINAD [dB] can be derived by $20 \times \log 10(1/Distortion)$.

c. The DistResidual term of the Distortion Accuracy specification contributes when the Reading term is small.

d. The measurement includes at most $10th$ harmonics.

e. AM rejection describes the instrument's FM reading for an input that is strongly AMed (with no FM); this specification includes contributions from residual FM.

f. Residual FM describes the instrument's FM reading for an input that has no FM and no AM; this specification includes contributions from FM deviation accuracy.

Amplitude Modulation

Conditions required to meet specification

- Depth: 1% to 99%
- Channel BW: \leq 1 MHz
- Rate: 50 Hz to 100 kHz
- SINAD bandwidth: (Channel BW) / 2
- Single tone sinusoid modulation

a. This specification applies to the result labeled "(Pk-Pk)/2".

b. Reading is a measured AM depth in %.

Amplitude Modulation

a. Channel BW is set to 15 times of Rate (Rate \leq 50 kHz) or 10 times the Rate (50 kHz < Rate \leq 100 kHz).

b. SINAD [dB] can be derived by $20 \times \log 10(1/D$ istortion).

c. FM rejection describes the instrument's AM reading for an input that is strongly FMed (and no AM); this specification includes contributions from residual AM

d. Residual AM describes the instrument's AM reading for an input that has no AM and no FM; this specification includes contributions from AM depth accuracy.

Phase Modulation

Conditions erquired to meet specification

- Peak deviation* : 0.2 to 100 rad
- \cdot Channel BW: \leq 1 MHz
- Rate: 20 Hz to 50 kHz
- SINAD bandwidth: (Channel BW) / 2
- Single tone sinusoid modulation

a. This specification applies to the result labeled "(Pk-Pk)/2".

b. For optimum measurement, ensure that the Channel BW is set wide enough to capture the significant RF energy. Setting the Channel BW too wide will result in measurement errors.

c. Reading is the measured peak deviation in radians.

^{*.}PeakDeviation (for phase, in rads) and Rate are jointly limited to fit within Channel BW. For PM, an approximate rule-of-thumb is 2 x [PeakDeviation + 1] x Rate < Channel BW; such that most of the sideband energy is within the Channel BW.

Phase Modulation

a. For optimum measurement, ensure that the Channel BW is set wide enough to capture the significant RF energy. Setting the Channel BW too wide will result in measurement errors.

b. SINAD [dB] can be derived by $20 \times \log 10(1/D$ istortion).

c. AM rejection describes the instrument's PM reading for an input that is strongly AMed (with no PM); this specification includes contributions from residual PM.

d. Residual PM describes the instrument's PM reading for an input that has no PM and no AM; this specification includes contributions from PM deviation accuracy.

Analog Out

The "Analog Out" connector (BNC) is located at the analyzer's rear panel. It is a multi-purpose output, whose function depends on options and operating mode (active application). When the N9063C Analog Demod application is active, this output carries a voltage waveform reconstructed by a real-time hardware demodulator (designed to drive the "Demod to Speaker" function for listening). The processing path and algorithms for this output are entirely separate from those of the N9063C application itself; the Analog Out waveform is not necessarily identical the application's Demod Waveform.

a. For AM, the output is the "RF envelope" waveform. For FM, the output is proportional to frequency-deviation; note that Carrier Frequency Error (a constant frequency offset) is included as a devi- ation from the analyzer's tuned center frequency, unless a HPF is used. For PM, the output is proportional the phase-deviation; note that PM is limited to excursions of +pi, and requires a HPF on to enable a phase-ramp-tracking circuit.

Most controls in the N9063C application do not affect Analog Out. The few that do are:

- * choice of AM, FM, or PM (FM Stereo not supported)
- * tuned Center Freq
- * Channel BW (affects IF filter, sample rate, and FM scaling)
- * some post-demod filters and de-emphasis (the hardware demodulator has limited filter choices; it will attempt to inherit the filter settings in the app, but with constraints and approximations)

The FM case has repeatable and deterministic scaling and offset behavior, and is continuous (smooth) through acquisition cycles. See above. The AM and PM cases are not, and should be used with caution.

FM Stereo/Radio Data System (RDS) Measurements

Analog Demodulation Measurement Application FM Stereo/Radio Data System (RDS) Measurements Phase Noise Measurement Application

Specification Guide

12 Phase Noise Measurement Application

This chapter contains specifications for the N9068C Phase Noise measurement application.

General Specifications

a. See Frequency Offset – Range.

a. This does not include the effect of system noise floor. This error is a function of the signal (phase noise of the DUT) to noise (analyzer noise floor due to phase noise and thermal noise) ratio, SN, in decibels.

The function is: $error = 10 \times log(1 + 10^{-SN/10})$

For example, if the phase noise being measured is 10 dB above the measurement floor, the error due to adding the analyzer's noise to the UUT is 0.41 dB.

- b. Offset frequency errors also add amplitude errors. See the Offset frequency section, below.
- c. The phase noise density accuracy is derived from warranted analyzer specifications. It applies with default settings and a 0 dBm carrier at 1 GHz. Most notable about the default settings is that the Overdrive (in the advanced menu of the Meas Setup menu) is set to Off.
- d. The accuracy of an RMS marker such as "RMS degrees" is a fraction of the readout. That fraction, in percent, depends on the phase noise accuracy, in dB, and is given by 100 \times (10^{PhaseNoiseDensityAccuracy / 20} - 1). For example, with +0.30 dB phase noise accuracy, and with a marker reading out 10 degrees RMS, the accuracy of the marker would be +3.5% of 10 degrees, or +0.35 degrees.

a. Standard deviation. The repeatability can be improved with the use of smoothing and increasing number of averages.

a. For example, f_{opt} is 3.0 GHz for *Option 503*.

b. The frequency offset error in octaves causes an additional amplitude accuracy error proportional to the product of the frequency error and slope of the phase noise. For example, a 0.01 octave frequency error combined with an 18 dB/octave slope gives 0.18 dB additional amplitude error.

Nominal Phase Noise at Different Center Frequencies

See the plot of basebox Nominal Phase Noise on page 42.

Noise Figure Measurement Application

Specification Guide

13 Noise Figure Measurement Application

This chapter contains specifications for the N9069C Noise Figure Measurement Application.

General Specification

a. The figures given in the table are for the uncertainty added by the CXA Signal Analyzer instrument only. To compute the total uncertainty for your noise figure measurement, you need to take into account other factors including: DUT NF, Gain and Match, Instrument NF, Gain Uncertainty and Match; Noise source ENR uncertainty and Match. The computations can be performed with the uncertainty calculator included with the Noise Figure Measurement Personality. Go to **Mode Setup** then select **Uncertainty Calculator**. Similar calculators are also available on the Keysight web site; go to http://www.keysight.com/find/nfu.

b. Uncertainty performance of the instrument is nominally the same in this frequency range as in the higher frequency range. However, performance is not warranted in this range. There is a paucity of available noise sources in this range, and the analyzer has poorer noise figure, leading to higher uncertainties as computed by the uncertainty calculator.

c. "Instrument Uncertainty" is defined for noise figure analysis as uncertainty due to relative amplitude uncertainties encountered in the analyzer when making the measurements required for a noise figure computation. The relative amplitude uncertainty depends on, but is not identical to, the relative display scale fidelity, also known as incremental log fidelity. The uncertainty of the analyzer is multiplied within the computation by an amount that depends on the Y factor to give the total uncertainty of the noise figure or gain measurement.

See Keysight App Note 57-2, literature number 5952-3706E for details on the use of this specification.

Jitter (amplitude variations) will also affect the accuracy of results. The standard deviation of the measured result decreases by a factor of the square root of the Resolution Bandwidth used and by the square root of the number of averages. This application uses the 4 MHz Resolution Bandwidth as default since this is the widest bandwidth with uncompromising accuracy.

a. "Instrument Uncertainty" is defined for gain measurements as uncertainty due to relative amplitude uncertainties encountered in the analyzer when making the measurements required for the gain computation. See Keysight App Note 57-2, literature number 5952-3706E for details on the use of this specification. Jitter (amplitude variations) will also affect the accuracy of results. The standard deviation of the measured result decreases by a factor of the square root of the Resolution Bandwidth used and by the square root of the number of averages. This application uses the 4 MHz Resolution Bandwidth as default since this is the widest bandwidth with uncompromising accuracy.

b. Uncertainty performance of the instrument is nominally the same in this frequency range as in the higher frequency range. However, performance is not warranted in this range. There is a paucity of available noise sources in this range, and the analyzer has poorer noise figure, leading to higher uncertainties as computed by the uncertainty calculator.

a. The Noise Figure Uncertainty Calculator requires the parameters shown in order to calculate the total uncertainty of a Noise Figure measurement.

b. Nominally, the noise figure of the spectrum analyzer is given by

 $NF = D - (K - L + N - B)$

where D is the DANL (displayed average noise level) specification,

K is kTB $(-173.98$ dB in a 1 Hz bandwidth at 290 K)

L is 2.51 dB (the effect of log averaging used in DANL verifications)

N is 0.24 dB (the ratio of the noise bandwidth of the RBW filter with which DANL is specified to an ideal noise bandwidth) B is ten times the base-10 logarithm of the RBW (in hertz) in which the DANL is specified. B is 0 dB for the 1 Hz RBW. The actual NF will vary from the nominal due to frequency response errors.

Noise Figure Measurement Application General Specification

Specification Guide

14 W-CDMA Measurement Application

This chapter contains specifications for the *N9073C* W-CDMA/HSPA/HSPA⁺ measurement application. It contains N9073C-1FP W-CDMA, N9073C-2FP HSPA and N9073C-3FP/HSPA⁺ measurement applications.

Additional Definitions and Requirements

Because digital communications signals are noise-like, all measurements will have variations. The specifications apply only with adequate averaging to remove those variations.

The specifications apply in the frequency range documented in In-Band Frequency Range.

Measurement

a. Absolute power accuracy includes all error sources for in-band signals except mismatch errors and repeatability due to incomplete averaging. It applies when the mixer level is high enough that measurement floor contribution is negligible.

a. The accuracy of the Adjacent Channel Power Ratio will depend on the mixer drive level and whether the distortion products from the analyzer are coherent with those in the UUT. These specifications apply even in the worst case condition of coherent analyzer and UUT distortion products. For ACPR levels other than those in this specifications table, the optimum mixer drive level for accuracy is approximately -37 dBm - (ACPR/3), where the ACPR is given in (negative) decibels.

W-CDMA Measurement Application Measurement

- b. To meet this specified accuracy when measuring mobile station (MS) or user equipment (UE) within 3 dB of the required -33 dBc ACPR, the mixer level (ML) must be optimized for accuracy. This optimum mixer level is -24 dBm, so the input attenuation must be set as close as possible to the average input power $-(-22$ dBm). For example, if the average input power is -6 dBm, set the attenuation to 16 dB. This specification applies for the normal 3.5 dB peak-to-average ratio of a single code. Note that if the mixer level is set to optimize dynamic range instead of accuracy, accuracy errors are nominally doubled.
- c. ACPR accuracy at 10 MHz offset is warranted when the input attenuator is set to give an average mixer level of 14 dBm (for all alternate channel and non-coherent ACPR).
- d. In order to meet this specified accuracy, the mixer level must be optimized for accuracy when measuring node B Base Transmission Station (BTS) within 3 dB of the required -45 dBc ACPR. This optimum mixer level is -18 dBm, so the input attenuation must be set as close as possible to the average input power $-(-18$ dBm). For example, if the average input power is -5 dBm, set the attenuation to 13 dB. This specification applies for the normal 10 dB peak-to-average ratio (at 0.01% probability) for Test Model 1. Note that, if the mixer level is set to optimize dynamic range instead of accuracy, accuracy errors are nominally doubled.
- e. Keysight measures 100% of the signal analyzers for dynamic range in the factory production process. This measurement requires a near-ideal signal, which is impractical for field and customer use. Because field verification is impractical, Keysight only gives a typical result. More than 80% of prototype instruments met this "typical" specification; the factory test line limit is set commensurate with an on-going 80% yield to this typical. The ACPR dynamic range is verified only at 2 GHz, where Keysight has the near-perfect signal available. The dynamic range is specified for the optimum mixer drive level, which is different in different instruments and different conditions. The test signal is a 1 DPCH signal.

The ACPR dynamic range is the observed range. This typical specification includes no measurement uncertainty.

f. 3GPP requires the use of a root-raised-cosine filter in evaluating the ACLR of a device. The accuracy of the passband shape of the filter is not specified in standards, nor is any method of evaluating that accuracy. This footnote discusses the performance of the filter in this instrument. The effect of the RRC filter and the effect of the RBW used in the measurement interact. The analyzer compensates the shape of the RRC filter to accommodate the RBW filter. The effectiveness of this compensation is summarized in three ways:

 White noise in Adj Ch: The compensated RRC filter nominally has no errors if the adjacent channel has a spectrum that is flat across its width.

 TOI-induced spectrum: If the spectrum is due to third-order intermodulation, it has a distinctive shape. The computed errors of the compensated filter are -0.004 dB for the 470 kHz RBW used for UE testing with the IBW method and also used for all testing with the Fast method, and 0.000 dB for the 30 kHz RBW filter used for BTS testing with the IBW method. The worst error for RBWs between these extremes is 0.05 dB for a 330 kHz RBW filter.

- rms CW error: This error is a measure of the error in measuring a CW-like spurious component. It is evaluated by computing the root of the mean of the square of the power error across all frequencies within the adjacent channel. The computed rms error of the compensated filter is 0.023 dB for the 470 kHz RBW used for UE testing with the IBW method and also used for all testing with the Fast method, and 0.000 dB for the 30 kHz RBW filter used for BTS testing. The worst error for RBWs between these extremes is 0.057 dB for a 430 kHz RBW filter.

a. The Complementary Cumulative Distribution Function (CCDF) is a reformatting of the histogram of the power envelope. The width of the amplitude bins used by the histogram is the histogram resolution. The resolution of the CCDF will be the same as the width of those bins.

a. The dynamic range specification is the ratio of the channel power to the power in the offset specified. The dynamic range depends on the measurement settings, such as peak power or integrated power. Dynamic range specifications are based on default measurement settings, with detector set to average, and depend on the mixer level. Default measurement settings include 30 kHz RBW.

b. This dynamic range specification applies for the optimum mixer level, which is about -16 dBm. Mixer level is defined to be the average input power minus the input attenuation.

c. The sensitivity is specified with 0 dB input attenuation. It represents the noise limitations of the analyzer. It is tested without an input signal. The sensitivity at this offset is specified in the default 30 kHz RBW, at a center frequency of 2 GHz.

d. The relative accuracy is a measure of the ratio of the power at the offset to the main channel power. It applies for spectrum emission levels in the offsets that are well above the dynamic range limitation.

e. The absolute accuracy of SEM measurement is the same as the absolute accuracy of the spectrum analyzer. See "Absolute [Amplitude Accuracy" on page 23](#page-22-0) for more information. The numbers shown are for 100 kHz to 3.0 GHz, with attenuation set to 10 dB.

a. This dynamic range is specified at 12.5 MHz offset from center frequency with mixer level of 1 dB compression point, which will degrade accuracy 1 dB.

b. The sensitivity is specified at far offset from carrier, where phase noise dose not contribute. You can derive the dynamic range at far offset from 1 dB compression mixer level and sensitivity.

a. ML (mixer level) is RF input power minus attenuation.

b. Code Domain Power Absolute accuracy is calculated as sum of 95% Confidence Absolute Amplitude Accuracy and Code Domain relative accuracy at Code Power level.

W-CDMA Measurement Application Measurement

a. ML (mixer level) is RF input power minus attenuation.

b. The accuracy specification applies when the EVM to be measured is well above the measurement floor and successfully synchronized to the signal. When the EVM does not greatly exceed the floor, the errors due to the floor add to the accuracy errors. The errors due to the floor are noise-like and add incoherently with the UUT EVM. The errors depend on the EVM of the UUT and the floor as follows: error = sqrt(EVMUUT 2 + EVMsa 2) — EVMUUT, where EVMUUT is the EVM of the UUT in percent, and EVMsa is the EVM floor of the analyzer in percent.

c. This specifies a synchronization range with CPICH for CPICH only signal.

d. $ta = transmitter frequency × frequency reference accuracy$

a. ML (mixer level) is RF input power minus attenuation.

b. For 16 QAM or 64QAM modulation, the relative code domain error (RCDE) must be better than -16 dB and -22 dB respectively.

c. The accuracy specification applies when the EVM to be measured is well above the measurement floor. When the EVM does not greatly exceed the floor, the errors due to the floor add to the accuracy errors. The errors due to the floor are noise-like and add incoherently with the UUT EVM. The errors depend on the EVM of the UUT and the floor as follows: error = [sqrt(EVMUUT 2 + $EVMsa²$] – EVMUUT, where EVMUUT is the EVM of the UUT in percent, and EVMsa is the EVM floor of the analyzer in percent. For example, if the EVM of the UUT is 7%, and the floor is 2.5%, the error due to the floor is 0.43%.

d. If 16 QAM and 64 QAM codes are included, it is not applicable.

e. This specifies a synchronization range with CPICH for CPICH only signal.

f. $ta = transmitter frequency × frequency reference accuracy$

g. The accuracy specification applies when the measured signal is the combination of CPICH (antenna-1) and CPICH (antenna-2), and where the power level of each CPICH is -3 dB relative to the total power of the combined signal. Further, the range of the measurement for the accuracy specification to apply is ± 0.1 chips.

In-Band Frequency Range

W-CDMA Measurement Application In-Band Frequency Range

Specification Guide

15 LTE/LTE-Advanced Measurement Application

This chapter contains specifications for the N9080C LTE/LTE-Advanced FDD measurement application and for the N9082C LTE/LTE-Advanced TDD measurement application.

Additional Definitions and Requirements

Because digital communications signals are noise-like, all measurements will have variations. The specifications apply only with adequate averaging to remove those variations.

The specifications apply in the frequency range documented in In-Band Frequency Range.

Measurements

a. Absolute power accuracy includes all error sources for in-band signals except mismatch errors and repeatability due to incomplete averaging. It applies when the mixer level is high enough that the measurement floor contribution is negligible.

a. This dynamic range expression is for the case of Information BW = 5 MHz; for other Info BW, the dynamic range can be derived. The equation is:

Dynamic Range = Dynamic Range for 5 MHz - $10*log_{10}(Info BW/5.0e6)$

a. Measurement bandwidths for mobile stations are 4.5, 9.0 and 18.0 MHz for channel bandwidths of 5, 10 and 20 MHz respectively.

b. The optimum mixer levels (ML) are -23, -23 and -23 dBm for channel bandwidths of 5, 10 and 20 MHz respectively.

c. Measurement bandwidths for base transceiver stations are 4.515, 9.015 and 18.015 MHz for channel bandwidths of 5, 10 and 20 MHz respectively.

d. The optimum mixer levels (ML) are -19, -18 and -18 dBm for channel bandwidths of 5, 10 and 20 MHz respectively.

e. The optimum mixer level (ML) is -14 dBm.

f. E-TM1.1 and E-TM1.2 used for test. Noise Correction set to On.

a. This dynamic range is specified at 12.5 MHz offset from center frequency with mixer level of 1 dB compression point, which will degrade accuracy 1 dB.

b. The sensitivity is specified at far offset from carrier, where phase noise dose not contribute. You can derive the dynamic range at far offset from 1 dB compression mixer level and sensitivity.

a. In these specifications, those values with % units are the specifications, while those with decibel units, in parentheses, are conversions from the percentage units to decibels for reader convenience.

b. The accuracy specification applies when EVM is less than 1% and no boost applies for the reference signal.

c. Requires *Option B25* (IF bandwidth above 10 MHz, up to 25 MHz).

d. The accuracy specification applies when the EVM to be measured is well above the measurement floor. When the EVM does not greatly exceed the floor, the errors due to the floor add to the accuracy errors. The errors due to the floor are noise-like and add incoherently with the UUT EVM. The errors depend on the EVM of the UUT and the floor as follows: error = [sqrt(EVMUUT2 + EVMsa2)] – EVMUUT, where EVMUUT is the EVM of the UUT in percent, and EVMsa is the EVM floor of the analyzer in percent.

e. $tfa =$ transmitter frequency \times frequency reference accuracy.

f. The accuracy specification applies when EVM is less than 1% and no boost applies for resource elements

In-Band Frequency Range

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